



journal homepage: http://jac.ut.ac.ir

# Vibration Analysis of Global Near-regular Mechanical Systems

Iman Shojaei<sup>\*1</sup> and Hossein Rahami<sup>†2</sup>

<sup>1</sup>Department of Biomedical Engineering, University of Kentucky, Lexington, KY 40506, USA. <sup>2</sup>School of Engineering Science, College of Engineering, University of Tehran, Tehran, Iran.

#### ABSTRACT

Some near-regular mechanical systems involve global deviations from their corresponding regular system. Despite extensive research on vibration analysis (eigensolution) of regular and local near-regular mechanical systems, the literature on vibration analysis of global nearregular mechanical systems is scant. In this paper, a method for vibration analysis of such systems was developed using Kronecker products and matrix manipulations. Specifically, the eigensolution of the corresponding regular mechanical system was inserted in the algorithm to further accelerate the solution. The developed method allowed reduction in computational complexity (i.e.,  $O(n^2)$ ) when compared to earlier methods. The application of the method was indicated using a simple example.

*Keyword:* Global near-regular systems; Vibration analysis, Eigensolution; Kronecker products; Matrix operations.

AMS subject Classification: 05C75.

#### **ARTICLE INFO**

Article history: Received 30, February 2017 Received in revised form 18, October 2017 Accepted 3 November 2017 Available online 01, December 2017

<sup>\*</sup>shojaei.iman@uky.edu

<sup>&</sup>lt;sup>†</sup>Corresponding author: Hossein Rahami. Email: hrahami@ut.ac.ir

### 1 Introduction

Vibration analysis and eigensolution of large-scale regular mechanical systems are performed using concepts from graph and group theories. The stiffness and mass matrices of such regular mechanical systems have canonical forms with specific repetitive or circulant block patterns allowing efficient eigensolution. Specifically, the power of these methods becomes more evident when analysis is to be repeated many times, for instance in dynamic design or non-linear analysis of regular mechanical systems. However, most mechanical systems do not exactly hold the pattern of a regular system such that the application of efficient eigensolutions are limited.

Some mechanical systems involve a small amount of irregularities wherein a small number of degrees of freedom are affected by the irregularity [5,7]. These mechanical systems with locally concentrated irregularities are called local near-regular systems, eigensolution of which has been obtained using modified numerical approaches [2]. Another group of mechanical systems involve global deviations (i.e., irregularity affects a large number of degrees of freedom) from their corresponding regular system and are called global near regular mechanical systems [1]. Eigensolution for these systems, however, has not been yet developed. Therefore, the objective of this paper was set to develop efficient methods for vibration analysis and eigensolution of mechanical systems with global near-regularity.

## 2 Vibration analysis of a global near-regular system

Developing a simple algorithm for the vibration analysis of global near-regular mechanical systems from available vibration solution of their corresponding regular mechanical systems is aimed.

Consider the given eigenproblem for a global near-regular system

$$Kx = \lambda Mx \tag{1}$$

where K is the stiffness matrix, x and  $\lambda$  are the eigenpairs, and M is the mass matrix. Assume  $\Delta K$  and  $\Delta M$  are the deviations of the stiffness and mass matrices of the nearregular system from the stiffness  $(K_{reg})$  and mass  $(M_{reg})$  matrices of the regular system.

$$K = K_{reg} + \Delta K$$
;  $M = M_{reg} + \Delta M$  (2)

And

$$K_{reg}x_{reg} = \lambda_{reg}M_{reg}x_{reg} \tag{3}$$

where  $x_{reg}$  and  $\lambda_{reg}$  are eigenpairs of the regular system. Substituting Eq. (2) in Eq. (1)

$$(K_{reg} + \Delta K) x = \lambda M x \tag{4}$$

Assume the eigenvector x can be approximated using a linear combination of m linearly independent basis vectors  $y_1, y_2, \cdots, y_m$ 

$$x_{(n\times 1)} = a_1 y_1 + a_2 y_2 + \dots + a_m y_m \quad \text{or} \quad x_{(n\times 1)} = Y_{(n\times m)} A_{(m\times 1)}$$
  
and 
$$Y = [y_1, y_2, \dots, y_m]_{(n\times m)} \quad ; \quad A^T = [a_1, a_2, \dots, a_m]_{(1\times m)}$$
(5)

where A is a vector of unknown coefficients. We set m to be much smaller than n (i.e., the number of degrees of freedom) and substitute Eq. (5) in Eq. (1)

$$Kx = \lambda Mx \to KYA = \lambda MYA \to Y^T KYA = \lambda Y^T MYA$$
  

$$K_r = Y^T KY \text{ and } M_r = Y^T MY \to K_r A = \lambda M_r A$$
(6)

where  $K_r$  and  $M_r$  are reduced stiffness and mass matrices of dimension m. Therefore, rather than solving a system of dimension n in Eq. (1), the smaller system of dimension m should be solved. Upon finding the vector A in Eq. (6), x is calculated from Eq. (5). However, the basis vectors are not determined yet.

Consider Eq. (4) and pre-multiply it by  $K_{reg}^{-1}$ 

$$(K_{reg} + \Delta K) x = \lambda M x \to (1+G) x = y_1 \tag{7}$$

where  $G = K_{reg}^{-1} \Delta K$  and  $y_1 = K_{reg}^{-1} \lambda M x$ . Therefore,

$$x = (1+G)^{-1} y_1$$

But, we can write

$$(1-G)\left(1+G+G^{2}+\dots+G^{r}\right) = 1-G^{r+1}$$
$$\left(1+G+G^{2}+\dots+G^{r}\right) = (1-G)^{-1}-(I-G)^{-1}G^{r+1}$$

Since  $(I - G)^{-1} G^{r+1} = 0$  as  $G^r \to 0$ , we have:

$$G \to -G : (I+G)^{-1} = (I-G+G^2-\cdots)$$
 (8)

Thus,

$$x = (I+G)^{-1}y_1 = (I-G+G^2-)y_1$$

Now assuming  $\lambda = \lambda_{reg}$  and  $x = x_{reg}$ 

$$y_1 = K_{reg}^{-1} \lambda M x = K_{reg}^{-1} \lambda_{reg} M x_{reg} \to y_1 = K_{reg}^{-1} R_{reg}$$

$$\tag{9}$$

Where  $R_{reg} = \lambda_{reg} M x_{reg}$ . Finally,

$$\begin{cases} y_i = -Gy_{i-1} \quad (i = 2:m) \\ y_1 = K_{reg}^{-1} R_{reg} \end{cases} \to x = \sum_{i=1}^m y_i \quad ; \ \lambda_j = \frac{x_j^T K x_j}{x_j^T M x_j} \tag{10}$$

For a regular mechanical system with given eigenpair matrices,  $\Lambda_{reg}$  and  $X_{reg}$ , decomposition of stiffness matrix would be  $K_{reg} = X_{reg}^T \Lambda_{reg} X_{reg}$  and  $y_1$  is solved as follows:

$$y_1 = \left(X_{reg}^T \Lambda_{reg} X_{reg}\right)^{-1} R_{reg} = X_{reg}^T \Lambda_{reg}^{-1} X_{reg} \lambda_{reg} M x_{reg}$$
(11)

With x and calculated from Eq. (10), we can update  $y_1$  (i.e.,  $R_{reg}$ ) and recalculate x and  $\lambda$  to achieve the desired accuracy. Also, same procedures should be conducted to calculate other eigenvalues and eigenvectors of the mechanical system.

Regardless of the required effort for defining the eigenpair matrices  $\Lambda_{reg}$  and  $X_{reg}$ , the solution of Eq. (10) includes matrix by vector multiplications of the computational complexity  $O(n^2)$ . However, the method is efficient only if there is a simple way to obtain  $\Lambda_{reg}$  and  $X_{reg}$ .

## 3 Decomposition of stiffness matrix of regular mechanical system

For a regular mechanical system full decomposition of stiffness matrix can be obtained using Kronecker products and matrix manipulations. The two general groups of decomposable regular mechanical systems include repetitive and circulant matrices with the following block patterns:

$$M_n = F_l(A_m, B_m, A_m) = I_l \otimes A_m + T_l \otimes B_m$$

$$M_n = G_l(A_m, B_m, A_m) = (P_1)_l \otimes A_m + (P_2)_l \otimes B_m + (P_3)_l \otimes B_m$$
(12)

where I is an identity matrix, T = F(0, 1, 0), and  $P_1$ ,  $P_2$  and  $P_3$  are permutation matrices. Using the following lemma, matrix M can be decomposed:

The sufficient condition for converting Hermitian matrices  $A_1$  and  $A_2$  into upper triangular matrices using one orthogonal matrix is [3]:

$$A_1 A_2 = A_2 A_1 \tag{13}$$

Let the matrix M be the sum of two (it can also be generalized to n Kronecker products) Kronecker products as  $M = A_1 \otimes B_1 + A_2 \otimes B_2$ . If F is the matrix that upper triangularizes the matrices  $A_1$  and  $A_2$ , then  $U = F \otimes I$  block upper triangularizes the matrix M, meaning that  $U^t M U$  is block upper diagonalized. Thus, we can write:

$$\lambda_M = \bigcup_{i=1}^l eig(M_i) \quad ; \quad M_i = \lambda_i(A_1)B_1 + \lambda_i(A_2)B_2 \tag{14}$$

where matrices  $A_1$  and  $A_2$  are of dimension l, and matrices  $B_1$  and  $B_2$  are of dimension m. Since IT = TI in Eq. (12) and considering that  $\lambda_{T_l} = 2 \cos \frac{k\pi}{l+1}$  [4], we will have

$$\lambda_M = \bigcup_{k=1}^{l} eig\left(2\cos\frac{k\pi}{l+1}B + A\right) \tag{15}$$

Permutation matrices also hold the following property:

$$P_i P_j = P_j P_i \tag{16}$$

The eigenpairs of the permutation matrix  $P_i$  are obtained as follows

$$\lambda = \left(e^{\frac{2\pi i}{l}}\right)^k = \omega^k \quad ; \quad i = \sqrt{-1} \quad ; \quad k = 0: l-1$$
$$\vartheta_k = \frac{1}{\sqrt{l}} (1, \omega_k, \omega_k^2, \cdots, \omega_k^{l-1})^T \tag{17}$$

And

$$\lambda_M = \bigcup_{k=1}^{l} eig\left(2\left(e^{\frac{2\pi i}{l}}\right)^{k-1}B + A\right)$$
(18)

The eigenvectors of matrix M are calculated through  $u \otimes v$  [6], where u is the eigenvector of  $A_2$  (T in Eq. (12)) and v is the eigenvector of  $B_1$ . With the obtained eigenpairs, we can decompose M as follows:

$$M = V^T \lambda V \tag{19}$$

Now, with  $\lambda$  and V in hand (i.e.,  $\Lambda_{reg}$  and  $X_{reg}$  in Eq. (11), Eq. (10) and Eq. (11) are solved.

#### References

- Kaveh, A., I. Shojaei, H. Rahami, New developments in the optimal analysis of regular and near-regular structures: decomposition, graph products, force method, Acta Mech, Vol. 226, No. 3, 665-681, (2015).
- [2] Kaveh, A. and H. Rahami, An efficient analysis of repetitive structures generated by graph products, International Journal for Numerical Methods in Engineering, No. 1, 84, 108-126, (2010).
- [3] Rahami, H., Kaveh, A., Shojaei, I., and Gholipour, Y. , Analysis of Irregular Structures Composed of Regular and Irregular Parts Using Graph Products, J. Comput. Civ. Eng., 28(4), (2014).
- [4] Shojaei, I., A. Kaveh and H. Rahami, Analysis of structures convertible to repeated structures using graph products, Computers and Structures, Vol. 125, 153-163, ( 2013).
- [5] Shojaei, I., A. Kaveh, H. Rahami, A Numerical Method for Eigensolution of Near-Regular Structural and Mechanical Systems, Periodica Polytechnica Civil Engineering, Vol. 60, Iss. 2, 247-255, (2016). Comput. 37 (2001), 101-114.
- [6] Shojaei, I., A. Kaveh, H. Rahami, R. Shirazi, B. Bazrgari, Analysis and reanalysis of mechanical systems: global near-regularity concept, Acta Mechania, 228(4), 14451456, (2017).

117

- 118 H. Rahami / JAC 49, issue 2 December 2017, PP. 113 118
  - [7] Yueh, W.-C.: Eigenvalues of several tridiagonal matrices. Applied Mathematics E-Notes. 5, 210-230 (2005).